



# <sup>W</sup>**Real-time Model Predictive Control of a Wastewater Treatment Plant based on Machine Learning**

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**Abstract:** In wastewater treatment two separate goals should be jointly pursued: nutrient removal and energy conservation. An efficient controller performance should cope with process uncertainties, seasonal variations and process nonlinearities. This paper describes the design and testing of a model predictive controller (MPC) based on neuro-fuzzy techniques, capable of estimating the main process variables and provide the right amount of aeration to achieve an efficient and economical operation. The algorithm has been field-tested on a large-scale municipal WWTP of about 500.000 PE with encouraging results in terms of better effluent quality and energy savings.

**Keywords:** Machine learning; Artificial Intelligence; Neuro-Fuzzy computing; Nutrient Removal; Model Predictive Control; Real-time Control

# **Introduction**

The goal of this study is the design and engineering of a real-time controller for nutrient removal, based on artificial intelligence (AI). The Wastewater Treatment Plant (WWTP) process scheme is shown in [Figure 1,](#page-0-0) where the dissolved oxygen (DO) set-point  $DO_{sp}$  and the recycle flow  $Q_r$  are determined on the basis of the future nutrient changes estimated by the artificial intelligence engine (AIE). The MPC manipulates these variables to reduce the amount of output total nitrogen and to minimise the energy consumption. The artificial intelligence engine predicts the future evolution of both ammonia and nitrate and on this basis the model predictive controller determines the DO set-point and the internal recycle.



<span id="page-0-0"></span>**Figure 1** Process scheme of the WWTP to which the MPC is applied.

The observed variables in this control scheme are the dissolved oxygen (DO) together with the Nitrogen species  $NH_4^+$  and  $NO_3^-$  in the oxidation tank. The controller outputs are the DO set-point and the internal recycle  $Q<sub>r</sub>$  expressed as a percentage  $(0 - 100\%)$  of the maximal allowable flow. The latter arrangement is due to the fact that the recycle pump operates at a fixed regime, so the percentage represents the fraction of the ON time in each time frame.





# W **Material and Methods**

The WWTP from which the data were acquired and which is being used as a test plant is the municipal plant of the city of Modena, in Northern Italy. It consists of a conventional nitrification/denitrification plant, as shown in [Figure 1,](#page-0-0) with a capacity of about 500,000 PE.

The process instrumentation consists of a Dissolved Oxygen meter and a nutrient sensor (Hach, Endress+Hauser). These field measurements are routed to the plant SCADA for real-time operation. An encrypted connection between the plant and the Energy Way centre was been created to allow prototypal test. This arrangement enables specific clients to access the controller through LAN. Through VPN encrypted tunnelling, clients can mount directories on the controller as NFS folders and obtain services directly from the controller, enabling fast analysis iteration and maintenance.

Communication between the centre and the plant SCADA is based on the Modbus protocol over TCP/IP, physically linking the controlling machine to the PLC-frontend with an Ethernet patch cable, enabling peer-to-peer IP communication.

The process variables are sampled at regular intervals  $\delta = 5$  min and the prediction and control horizons were suitably defined as  $\alpha$  and  $\beta$  multiples of  $\delta$  respectively, which cannot be specified here for industrial confidentiality. The AI components of the MPC were trained and validated using plant data spanning over one year of operation.

The proposed model predictive controller (EW stands for Energy Way) is shown in [Figure 2](#page-1-0) where in the lower block a set of neuro-fuzzy networks forecasts the relevant process variables α steps ahead, while the upper block implements a heuristic search procedure to select the most appropriate value of the DO set-point β steps ahead.



<span id="page-1-0"></span>

It consists of two main parts: the prediction of the future process variables (lower block) and the heuristic search of the "best" input to be applied at the next step (upper block). Unlike many industrial processes where an approximating linear model can be obtained, WWTP is a highly nonlinear, time-varying process. For this reason *ad-hoc*  versions of MPC have been devised (Marsili-Libelli and Giunti, 2002; Hong and Bhamidimarri, 2003; Holenda et al., 2008; O'Brien et al., 2011; Han et al., 2014; Yang et al., 2014; Francisco et al., 2015; Mulas et al., 2015; Foscoliano et al., 2016; Goldar et al., 2016; Haimi et al., 2016; Marsili-Libelli, 2016; Han et al., 2017).





Another aspect of WWTP management, is the harmonisation of two control objectives to balance the effluent quality requirements with the energy conservation (Flores et al., 2007; Hakanen et al., 2013; Han and Qiao, 2014; Mustapha et al., 2018; Qiao et al., 2018; Torregrossa et al., 2018). In our controller, shown in [Figure 2](#page-1-0) the predictive section (lower block) is implemented as a set of neuro-fuzzy networks (Jang, 1993; Jang et al., 1998) further modified by Marsili-Libelli, (2016) and Bartoletti et al., (2018) while the predictive controller (upper block) is based on a heuristic search which selects the best future air flow  $U_a^*(t + \alpha)$  as the one which yields the DO value closest to the future set-point  $DO_{sp}^{*}( t + \alpha )$ , by testing an array of input values. In details, the neuro-fuzzy networks shown in [Figure 3](#page-2-0) forecast the nutrient concentrations at  $\alpha$  steps ahead, while [Figure 4](#page-2-1) shows how this information is repeatedly used by the heuristic search engine to compute the best air flow, as described earlier. So while the prediction horizon is  $\alpha$  steps ahead, the control horizon is β step ahead for the DO set-point and the air flow, with  $β < α$ .



<span id="page-2-0"></span>**Figure 3** Neuro-fuzzy networks to predict the future outputs (lower block of [Figure 2\)](#page-1-0).

<span id="page-2-1"></span>**Figure 4** Inverse network to select the best input by heuristic search (upper block of [Figure 2\)](#page-1-0).

The prediction accuracy is assessed through the following performance indexes

$$
MAE (Mean Absolute Error) = \frac{1}{n} \sum_{i=1}^{n} |\hat{y}_i - y_i| \quad RAE (Relative Absolute Error) = 100 \times \frac{1}{n} \sum_{i=1}^{n} \left| \frac{\hat{y}_i - y_i}{y_i} \right| , \tag{1}
$$

where y represents the actual generic variable and  $\hat{y}$  its estimate. The inverse network of [Figure 4](#page-2-1) computes the next DO set-point at each time step by minimising the following weighted sum of process variables as the following objective function which takes into account both the predicted process variables (Nitrogen species) and the energy consumption, represented by the blower energy.

$$
DO_{\varphi}^{*}(t+\beta) = \min_{D_{O_{\varphi}}} \left[ \gamma_{i} \frac{N\hat{H}_{i}^{*}(t+\alpha) + N\hat{O}_{i}(t+\alpha)}{\overline{N}_{\text{tot}}} + \gamma_{2} \frac{E(t+\beta)}{\overline{E}} + \right]
$$
  
\n
$$
DO_{\varphi}^{*}(t+\beta) = \min_{D_{O_{\varphi}}} \left[ \gamma_{3} \frac{DO_{\varphi}(t+\beta) - DO_{\varphi}(t)}{\overline{DO_{\varphi}}} + \rho_{1} \frac{N\hat{H}_{i}(t+\alpha)}{\overline{NH}_{i}} + \right]
$$
  
\nwhere  
\n
$$
N_{\text{tot}} = NH_{i}^{+} + NO_{j}^{-}
$$
  
\n
$$
N_{\text{tot}} = NH_{i}^{+} + NO_{j}^{-}
$$
  
\n
$$
N_{\text{tot}} = \sum_{i=1}^{N} N\hat{O}_{i} \frac{P_{i}^{*}(t+\alpha)}{\overline{NO_{i}}} + \rho_{3} \frac{\hat{N}_{\text{tot}}(t+\alpha)}{\overline{N}_{\text{tot}}}
$$
  
\n
$$
\overline{N}_{\text{tot}} = \sum_{i=1}^{N} N\hat{O}_{i} \tag{2}
$$
  
\n
$$
N_{\text{tot}} = N\hat{H}_{i}^{*} + NO_{j}^{-}
$$
  
\n
$$
\overline{N}_{\text{tot}} = \text{overage value}; \alpha = \text{prediction horizon}; \beta = \text{control horizon}
$$





While the constraints with the  $\gamma$  weights are always active, those with the  $\rho$ coefficients are engaged whenever the pertinent variable activates its constraint, namely

$$
\rho_1 \neq 0 \quad \text{if} \quad N\hat{H}_4(t+\alpha) \geq NH_4^*
$$
\n
$$
\rho_2 \neq 0 \quad \text{if} \quad N\hat{O}_3(t+\alpha) \geq NO_3^*
$$
\n
$$
\rho_3 \neq 0 \quad \text{if} \quad \hat{N}_{\text{tot}}(t+\alpha) \geq N_{\text{tot}}^*
$$
\n
$$
\text{with } NH_4^*, NO_3^*, N_{\text{tot}}^* \quad \text{fixed threshold values}
$$
\n
$$
(3)
$$

The recycle flowrate is then updated according to the forecasted process variables

$$
Q_{r}(t+\beta) = Q_{r}(t) + \frac{N\hat{O}_{s}(t+\alpha) - N\hat{O}_{s}(t)}{N\hat{O}_{s}(t)} \Rightarrow \begin{cases} Q_{r}(t+\beta) = \min(Q_{r}(t+\beta),100) \\ Q_{r}(t+\beta) = \max(60,Q_{r}(t+\beta)) \end{cases}
$$
(4)

#### **Results and Discussion**

The estimated process variables at the end of the prediction horizon  $(t, t+\alpha)$  provided by the trained neuro-fuzzy predictors are shown in [Figure 5](#page-3-0) while the improvement in effluent quality and energy saving are shown in [Figure 7](#page-4-0) and in [Table 1.](#page-4-1)



<span id="page-3-0"></span>**Figure 5** Preliminary off-line prediction of the process variables at time t+ $\alpha$  for the nutrients and at t+ $\beta$ for the air flow provided by the trained neuro-fuzzy networks. Normalised values are shown for confidentiality.

A sensitivity assessment was then performed on the model by observing the variations of the output variables  $(NH_4^*, NO_3^-)$  caused by a  $\pm 20\%$  variation in DO. [Figure 6a](#page-3-1) shows that a positive DO variation of 20% produces a  $NH<sub>4</sub><sup>+</sup>$  decrease in 95.8% of the cases (red bars), while a -20% DO variation results in an increase of  $NH<sub>4</sub>$  in 96.1% of the times (blue bars). Likewise, [Figure 6b](#page-3-1) shows that a +20% DO increase is followed by an  $NO_3^-$  increase in 91.7% of the cases, while a -20% DO decrease results in a lower  $NO_3^-$  in 92.3 % of the times. The spread in the response is due to the influence of other process conditions.



<span id="page-3-1"></span>**Figure 6** Sensitivity assessment of the predictive model of [Figure 3.](#page-2-0) The ammonium-N variations in response to a 20% change in DO are shown in (a), while (b) shows the corresponding changes in





nitrate-N. Notice the inverted response of the two output variables.

After testing the consistency of the predictions via sensitivity analysis the proposed MPC has been compared with the conventional controller (CC) previously in operation. The total Nitrogen  $(N_{tot})$  comparison of [Figure 7](#page-4-0) shows that the EW controller, operating between samples 190 and 300, can keep the output  $N_{tot}$  lower than the conventional one.



<span id="page-4-0"></span>**Figure 7** Comparison of total-N output with the conventional and EW controller, operating between samples 190 and 300 (shaded area) corresponding to the period of test in March 2019. A lower  $N_{tot}$ output was obtained by the EW controller.

Based on this encouraging result, [Table 1](#page-4-1) shows the improvement obtained with the EW controller after an extended run in March 2019.

<span id="page-4-1"></span>**Table 1** Performance improvement achieved by our predictive controller (EW) over the conventional controller (CC) represented by the shaded area in [Figure 7.](#page-4-0)

	Measured averages				Estimated
					average
	Ammonium-N	Nitrate-N	<b>Total-N</b>	Air Flow	Electric power
Δ(EW-CC)	+2.8%	$-7.6%$	$-5.1%$	-10.7%	$-10.4\%$

Two more test runs are now examined, each optimised according to a differing objective. In the first test the emphasis was placed on the effluent quality during a high-load period and the results are shown in [Figure 8.](#page-5-0)

In [Figure 8a](#page-5-0) the DO set-point varies according to the predicted treatment requirements, computed by the forecasting engine of [Figure 4,](#page-2-1) and the DO controller operates in such a way to maintain the DO level close to its set point. [Figure 8b](#page-5-0) shows the corresponding airflow variations, providing more air flow whenever the organic load increases. In particular it can be seen that around samples 1500 and 3400 the DO set-point was raised to cater for the increased treatment demand. The other airflow fluctuations are a consequence of the controller reaction to the varying load, which requires differing level of air flow to track the DO set-point. [Figure 8c](#page-5-0) shows that the predicted N<sub>tot</sub> is very close to the measured value at all times. The reliability of the forecasting engine of [Figure 4](#page-2-1) is at the basis of the successful controller of [Figure 3.](#page-2-0) Further, the two DO peaks at samples 1500 and 3400 correspond to an increased organic load, as reflected by the two  $N_{\text{tot}}$  peaks.







<span id="page-5-0"></span>**Figure 8.** Output process variables during a high-load test period during which the output quality was optimised. (a) DO vs. DO set-point; (b) Airflow; (c) Comparison between predicted and measured total N (normalised).



**Figure 9** Relative weights in the loss function eq. (1) during the run of [Figure 8.](#page-5-0)

<span id="page-5-1"></span>[Figure 9](#page-5-1) shows the relative weights of the loss function during the quality effluent optimisation. The blue bars, corresponding to the unconstrained  $N_{\text{tot}}$  term, are comparatively larger than any other one, indicating that the emphasis is primarily placed on the minimisation of the output Nitrogen. The green bars show that the further constraint on  $N_{tot}^*$  is also activated most of the time, because the Nitrogen values are near the high end of the allowable band.



<span id="page-5-2"></span>**Figure 10** Relative weights in the loss function under the energy conservation objective.





Conversely, when the organic load is below its critical level the emphasis is placed on limiting the energy consumption. [Figure 10](#page-5-2) shows the new arrangement of the weights in the loss function (2) with more emphasis being placed on the unconstrained energy term ( $\gamma_2$ ), while the variable weights ( $\rho_1$ ,  $\rho_2$ ,  $\rho_3$ ) are never engaged, given the low value of the organic load.

From the previous performance figures it can be seen that the controller is able to switch between these two operational modes and selects the objective to be pursued depending on the incoming load estimated by the predictor of [Figure 3.](#page-2-0) In fact, the two loss functions of [Figure 9](#page-5-1) and [Figure 10](#page-5-2) were produced at different times by the same controller which dynamically adapts its objective function depending on the present and predicted loading conditions. As shown, during high-load periods the emphasis is placed on the output quality, while in low-load condition energy conservation becomes the main goal. A blend of these two objectives is achieved by the comprehensive loss function (2) where the variable weights ( $\rho_1$ ,  $\rho_2$ ,  $\rho_3$ ) contribute to the optimal target only under certain circumstances.

## **Conclusions**

This paper has described the design and field testing of the EW MPC based on neurofuzzy networks and heuristic search. Its key aspect is the ability to predict sufficiently in advance ( $\alpha > 30$  min) the N<sub>tot</sub> peaks, thus anticipating the required values of dissolved oxygen and air flow to secure safe effluent standards and thus saving energy and improving the effluent quality. The forecast performances of the neuro fuzzy models obtained during the offline test were also maintained during closed-loop realtime operation, as shown in [Figure 8c](#page-5-0).

During the initial test the two controllers (EW and CC) were alternatively engaged as shown in Figure 7. The good performance obtained with EW controller [\(Table 1\)](#page-4-1) with respect to the two management goals (effluent quality and energy conservation) eventually led to the decision of adopting the EW controller on a permanent basis. The flexibility of the controller is also demonstrated by comparing the relative weights of the loss function (2) in two periods with differing treatment requirements, as demonstrated in [Figure 9](#page-5-1) and [Figure 10.](#page-5-2) The system is presently in operation at the plant described, where it has replaced the previous conventional controller.

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