



UNIVERSITÀ
DEGLI STUDI
FIRENZE

FLORE

Repository istituzionale dell'Università degli Studi di Firenze

Influence of flight altitude and control points in the georeferencing of images obtained by unmanned aerial vehicle

Questa è la Versione finale referata (Post print/Accepted manuscript) della seguente pubblicazione:

Original Citation:

Influence of flight altitude and control points in the georeferencing of images obtained by unmanned aerial vehicle / Lucas Santos Santana; Gabriel Araújo e Silva Ferraz; Diego Bedin Marin; Brenon Dienevam Souza Barbosa; Luana Mendes dos Santos; Patrícia Ferreira Ponciano Ferraz; Leonardo Conti; Stefano Camiciottoli; Giuseppe Rossi. - In: EUROPEAN JOURNAL OF REMOTE SENSING. - ISSN 2279-7254. -

Availability:

The webpage <https://hdl.handle.net/2158/1215922> of the repository was last updated on 2021-04-12T12:32:40Z

Published version:

DOI: 10.1080/22797254.2020.1845104

Terms of use:

Open Access

La pubblicazione è resa disponibile sotto le norme e i termini della licenza di deposito, secondo quanto stabilito dalla Policy per l'accesso aperto dell'Università degli Studi di Firenze (<https://www.sba.unifi.it/upload/policy-oa-2016-1.pdf>)

Publisher copyright claim:

La data sopra indicata si riferisce all'ultimo aggiornamento della scheda del Repository FloRe - The above-mentioned date refers to the last update of the record in the Institutional Repository FloRe

(Article begins on next page)

Influence of flight altitude and control points in the georeferencing of images obtained by unmanned aerial vehicle

Journal:	<i>European Journal of Remote Sensing</i>
Manuscript ID	TEJR-2020-0096.R3
Manuscript Type:	Original Paper
Date Submitted by the Author:	28-Oct-2020
Complete List of Authors:	Santos Santana, Lucas; Federal University of Lavras Department of Engineering, Department of Agricultural Engineering Araújo e Silva Ferraz, Gabriel; Federal University of Lavras Department of Engineering, Department of Agricultural Engineering Bedin Marin, Diego; Federal University of Lavras Department of Engineering, Department of Agricultural Engineering Dienevam Souza Barbosa, Brenon; Federal University of Lavras Department of Engineering, Department of Agricultural Engineering Mendes dos Santos, Luana; Federal University of Lavras Department of Engineering, Department of Agricultural Engineering Ferreira Ponciano Ferraz, Patricia; Federal University of Lavras Department of Engineering, Department of Agricultural Engineering Camiciottoli, Stefano; UniFi DAGRI COnti, Leonardo; UniFi DAGRI rossi, giuseppe; UniFi DAGRI
Keywords:	remote sensing, RPA, flight parameters, image georeferencing, UAS
Abstract:	<p>This study aimed to explore the influence of flight altitude, density, and distribution of ground control points (GCPs) on the digital terrain model (DTM) in surveys conducted by unmanned aerial vehicles (UAVs). A total of 144 photogrammetric projects consisting of 399 aerial photos were carried out in a 2 ha area. These photogrammetric projects involved six GCP distributions (edge, center, diagonal, parallel, stratified, and random), six GCP densities, and four flight altitudes (30, 60, 90, and 120 m). The response surface methodology was used to find interference factors and total root mean square error (RMSEt) as well. The 60 m flight altitude presented was the most efficient, as it collected more images in less time. Central GCP distribution was observed to have low precision. Using stratified and random edge distributions, 10 GCPs are recommended to achieve geometric precision below 0.07 m at any flight height. However, for studies requiring up to 0.07 m precision, the best distribution was parallel with 4 GCPs at any altitude. Diagonal positioning of the GCPs showed RMSEt values below 0.11 m with 4 GCPs at any altitude. In the graphs of the response surface, an equation is presented regarding estimating error before the flight. A good distribution of GCPs was found to be important, but the density of GCPs per image was more relevant when obtaining a lower RMSEt.</p>

1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60



SCHOLARONE™
Manuscripts

1
2
3
4 **Influence of flight altitude and control points in the georeferencing of**
5 **images obtained by unmanned aerial vehicle**
6
7

8
9 Lucas Santos Santana^a, Gabriel Araújo e Silva Ferraz^a, Diego Bedin
10
11 Marin^a, Brenon Dienevam Souza Barbosa^a, Luana Mendes dos Santos^a,
12
13 Patrícia Ferreira Ponciano Ferraz^a, Leonardo Conti^b Stefano Camiciottoli^b
14
15 and Giuseppe Rossi^{b*}
16

17
18 *^aDepartment of Engineering, Federal University of Lavras - UFLA, Aqueanta Sol, 3037*
19 *Lavras - MG, Brazil; ^bDepartment of Agriculture, Food, Environment and Forestry*
20 *(DAGRI), University of Florence, Via San Bonaventura, 13 – 50145, Florence, Italy.*
21
22

23
24 *corresponding author: giuseppe.rossi@unifi.it
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60

Abstract

This study aimed to explore the influence of flight altitude, density, and distribution of ground control points (GCPs) on the digital terrain model (DTM) in surveys conducted by unmanned aerial vehicles (UAVs). A total of 144 photogrammetric projects consisting of 399 aerial photos were carried out in a 2 ha area. These photogrammetric projects involved six GCP distributions (edge, center, diagonal, parallel, stratified, and random), six GCP densities, and four flight altitudes (30, 60, 90, and 120 m). The response surface methodology was used to find interference factors and total root mean square error (RMSEt) as well. The 60 m flight altitude presented was the most efficient, as it collected more images in less time. Central GCP distribution was observed to have low precision. Using stratified and random edge distributions, 10 GCPs are recommended to achieve geometric precision below 0.07 m at any flight height. However, for studies requiring up to 0.07 m precision, the best distribution was parallel with 4 GCPs at any altitude. Diagonal positioning of the GCPs showed RMSEt values below 0.11 m with 4 GCPs at any altitude. In the graphs of the response surface, an equation is presented regarding estimating error before the flight. A good distribution of GCPs was found to be important, but the density of GCPs per image was more relevant when obtaining a lower RMSEt.

Keywords: remote sensing; RPA; flight parameters; image georeferencing; UAS

Introduction

Precision agriculture is a useful model in the management of natural resources and improvement of modern agriculture. (Orozco & Llano Ramírez, 2016; Far & Rezaei-Moghaddam, 2018). Among precision agriculture techniques, aerial remote sensing presents new methods of research and work optimization, capturing terrestrial features using unmanned aerial vehicles (UAVs). Some applications of UAVs in agriculture were presented in studies of variables related to nitrogen in corn (Corti et al., 2019), the evaluation of water stress in agriculture (Gago et al., 2015), and precision agriculture (Mogili & Deepak, 2015).

Image collection using UAVs and their photogrammetric applications offers the possibility to observe agricultural fields from a different point of view. Therefore, it is possible to observe some field aspects that are relatively invisible when monitored from the ground (Candiago, Remondino, De Giglio et al., 2015; Polo, Hornero, Duijneveld et al., 2015; Rodríguez-Fernández, Menéndez & Camacho et al., 2017). In addition, UAVs offer other advantages, such as flexibility in collecting images, improved spatial resolution, and control over temporal resolution.

With the advent and popularization of UAVs for agricultural applications, photogrammetry has garnered interest and become one of the most modern technologies in crop management. However, it should be considered that the orthomosaic generated by aerial images presents geometric errors, which can be attenuated according to the terrain slope, image overlap, crop type, and flight altitude. Parameters such as image overlap and flight altitude are considered essential to optimize UAV flight missions. Variations in flight altitude are required in order to fly efficiently and faster.

Flight time is considered an important parameter to define flight plans, in some cases even compromising the study. One of the restrictions of aerial sensing using UAVs is the flight range (Traub 2011). Aside from the work described in Ma, Zhang, &

1
2
3 Xu (2013), Deery, Jimenez-Berni, Jones et al. (2014) and Erdelj, Saif, Natalizio et al.
4
5 (2017) explained that electric UAVs are unable to operate for long periods due to
6
7 limited battery capacity. Commercial rotary wing-type UAVs typically achieve 25–30
8
9 min flights, thereby limiting continuous operation and large-scale coverage.

10
11
12 The general objective of photogrammetry is to represent characteristics of a
13
14 surface with reliability in terms of precision and accuracy. (Daakir, Pierrot-Deseilligny,
15
16 Bosser et al., 2016; Jalandoni, Domingo & Taçon 2018). Photogrammetric
17
18 reconstruction can be performed using software that applies structure from motion
19
20 (SfM) algorithms (Izumida, Uchiyama, & Sugai 2017).
21
22

23
24 Among the photogrammetric techniques based on images, structure from motion
25
26 (SfM) is one of the most used (Rahaman & Champion 2019). With 2D images, epipolar
27
28 geometry is estimated with resource matching algorithms, for example, the SIFT scale-
29
30 invariant feature transform (SIFT) algorithm (Ding, Zheng, Zhou et al., 2018). This
31
32 technique can be used to estimate external orientation on images and 3D object
33
34 geometry reconstruction (Brandolini & Patrucco 2019). Some approaches in the
35
36 literature emphasize the capacity of SfM in the generation of digital elevation models
37
38 (DEMs) (Castillo, Pérez, James et al., 2012).
39
40

41
42 On the other hand, research indicated that there may be systematic deformations
43
44 in UAV images (Rosnell & Honkavaara, 2012). In UAV applications, cameras
45
46 generally capture images vertically and move parallel to the floor. Near-parallel
47
48 imaging conditions and inaccurate self-calibration of unknown radial distortion can
49
50 produce distorted reconstruction results (Li, Cai, Wen et al., 2016). These errors are
51
52 known as a central domain (doming effect) and interfere with the geometric quality of
53
54 the orthomosaic (Javernick, Brasington & Caruso et al., 2014). The doming effect is a
55
56 fundamental problem of digital surface model (DSM) generation by SfM analysis
57
58
59
60

1
2
3 associated with sets of almost parallel images and inaccurate correction of radial
4
5 distortion of the lens (James & Robson 2014).
6

7
8 There are two paths to achieving high precision in aerial surveys, i.e., aircraft
9
10 equipped with real-time kinematic (RTK) systems or ground control points (GCPs)
11
12 (Chiang, Tsai, & Chu 2012; Tsai & Lin, 2017). GCPs can be obtained using a
13
14 topographic or geodetic survey of points, for example, by using a total station or a pair
15
16 of high-precision global navigation satellite system (GNSS) receivers. This method can
17
18 support the georeferencing of data and geometric correction of images captured by
19
20 UAVs, which are characterized as clearly visible reference targets in aerial images
21
22 (Agüera-Vega, Carvajal-Ramirez, Martínez-Carricondo et al., 2018).
23
24

25
26 Studies such as those performed by Brunier, Fleury, Anthony et al. (2016) with
27
28 real-time kinematic differential GPS (RTK-DGPS) and a total station generally prove to
29
30 be of high precision and accuracy. However, this method requires a high spatial density
31
32 of points to construct the digital elevation model (DEM); therefore, this type of work
33
34 requires time, which increases the cost of the project. Ribeiro-Gomes, Hernandez-
35
36 Lopez, Ballesteros et al. (2016) reported that the manual tasks needed to generate
37
38 geometric products control the price of projects. Tasks such as walking in a field to
39
40 collect points can slow a survey and require more than one operational professional,
41
42 making the project more expensive.
43
44
45

46
47 The tracking system in a UAV consists of a GNSS receiver that provides its
48
49 absolute location in the SIRGAS 2000 system. Because it is a navigation receiver, it
50
51 produces a minimum error, in the order of meters (Zhang & Hsu, 2018). Errors in the
52
53 range of meters are expected in GNSS receivers that collect only L1 data frequency.
54
55 Differential GNSS (DGNSS) systems receive signals via two antennae of L1 and L2
56
57 frequency, thus collecting data from more satellites, increasing the number of
58
59
60

1
2
3 triangulations, and improving precision and accuracy (Pervan, Chan, Gebre-Egziabher
4
5 et al., 2003).

6
7
8 Although control points bring geometric quality to the orthomosaic, some GCP
9
10 investigations remain somewhat controversial, causing few studies to use this technique.
11
12 In some cases, incorrect distribution and quantity of GCPs are used, i.e., the same
13
14 precision could be achieved with a reduced number of points combined with adequate
15
16 flight planning taking into consideration the photo scale, camera calibration, and flight
17
18 project specification. Few studies in the literature correlate the influence of UAV flight
19
20 altitude and the distribution and density of GCPs.
21
22

23
24 The time required for fieldwork is significantly optimized by the reduction of
25
26 the number of GCPs (Eisenbeiss & Sauerbier 2011). To increase the reliability of some
27
28 variables such as flight efficiency and geometric precision in the orthomosaic it is
29
30 essential to know the GCP distribution associated with the flight parameters. An
31
32 efficient flight captures more images in less flight time maintaining acceptable
33
34 geometric errors; this could decrease fieldwork time and accelerate project execution.
35
36

37
38 Therefore, this study aimed to evaluate the influence of the density of GCPs
39
40 allocated in different distributions and submitted to different flight altitudes to assess
41
42 the geometric precision, flight efficiency, and number of images in surveys conducted
43
44 by UAVs.
45
46

47 48 **Materials and Methods**

49
50
51 The methodology used in this work involves data collection steps via UAV and GNSS
52
53 receivers, data processing, and interpretation of results. The processes of obtaining
54
55 results are shown in flowchart form (Figure 1) and detailed in the following sections.
56
57

58 [Figure 1 near here]
59
60

Study Area

The study was conducted in an experimental area consisting of coffee crops at the Federal University of Lavras (UFLA) (Figure 2), located in the municipality of Lavras, state of Minas Gerais, Brazil, covering an area of 2 ha with the geographical coordinates 21°13'33.23" south and 44°58'17.63" west.

[Figure 2 near here]

Acquisition of Georeferenced Data

The equipment used for data collection in the field is presented in Figure 3. In this area, 43 GCPs, pre-defined in a grid with 25 × 25 m intersections, were georeferenced with high precision and fixed in the field. The points were accurately obtained with an error of less than 0.03 m using a pair (base and rover) of GNSS antennas (Figure 3A), Spectra Precision model SP60, operating in a real-time kinematic model (RTK).

[Figure 3 near here]

To characterize and identify the GCPs, 0.3 × 0.3 m targets as shown in Figure 3C were placed at each tracked point obtained through the GNSS receivers. These GCPs were used to georeference the images obtained by the UAV.

EZSurv software and a digital platform of the Brazilian Institute of Geography and Statistics (IBGE) were used in order to process the collected points. This process consisted of transforming signals received between satellites and GNSS equipment into coordinates. To improve precision, the geographic coordinates (X, Y, and Z) from the RTK base were sent to the IBGE and adjusted by precise point positioning (PPP). Table 1 presents coordinates processed in the system of PPP. This positioning method applies

1
2
3 an orbit and clock correction in the GNSS. Its main benefit concerning differential
4 positioning techniques is its ability to provide a position within a global reference frame
5
6 anywhere in the world with a single GNSS receiver (Grinter & Roberts, 2011).
7
8

9
10 [Table 1 near here]
11

12 The coordinates obtained with the GNSS in rover mode were processed after
13 processing the base coordinates, as shown in Figure 4. At this stage, the data between
14 the GNSS base and GNSS rover were aligned in order to adjust the collected data
15 precision. EZSurv eliminated faulty incoming signals to achieve greater precision.
16
17
18
19
20

21 [Figure 4 near here]
22
23
24

25 *Acquisition of Photogrammetric Data*

26 The aerial images were obtained with a DJI Phantom 4 Advanced aircraft as shown in
27 Figure 3B, with the following characteristics: weight, 1,388 g; size, 350 mm; maximum
28 speed, 72 km/h; maximum angle of inclination, 42°; maximum flight time, 30 min. The
29 GPS/GLONASS positioning system was equipped, by default, with a 1 inch CMOS
30 sensor to capture video (up to 4,096 × 2,160 p at 60 fps) and photos up to 20
31 megapixels.
32
33
34
35
36
37
38
39
40

41 With the targets positioned at the tracking sites, the flight missions began. The
42 planning was performed using the free software Drone Deploy installed on an Android
43 6.0 system. The flight plan was defined according to the following characteristics:
44 speed, 3 m/s; front and side overlap, 60% × 80%, respectively; flight direction bearing,
45 50°; area, 2 hectares. The same mission was applied to the different altitudes of 30, 60,
46 90, and 120 meters.
47
48
49
50
51
52
53
54

55 Six different CGP distributions were defined: random, edge, center, diagonal,
56 parallel, and stratified, as shown in Figure 5. The distributions were combined with
57
58
59
60

1
2
3 variations in GCP density and different flight altitudes, forming a final combination that
4
5 evaluated six distributions of 4, 5, 8, 10, 14, and 20 GCPs and flight altitudes of 30, 60,
6
7 90, and 120 m, totaling 399 aerial photos and 144 photogrammetric projects.
8
9

10 [Figure 5 near here]
11
12

13 ***Processing of Photogrammetric Data***

14
15
16 Photogrammetric processing was performed using Agisoft PhotoScan software, version
17
18 1.4.3. According to Sona, Pinto, Pagliari et al. (2014), this software, which is based on
19
20 an SfM algorithm, is superior to others in terms of precision. It uses multiple camera
21
22 views to increase photogrammetric data accuracy, not so different from aerial or
23
24 terrestrial LiDAR. It can provide three-dimensional points and produces a reliable data
25
26 set to create dense point clouds. The input photographs can then be mosaicked and
27
28 orthorectified to create the DEM by converting the point clouds into vector mesh or
29
30 raster digital elevation models (DEMs) (Dietrich 2016).
31
32
33

34
35 The methodology adopted by Flynn & Chapra (2014) and Rusnák, Sládek,
36
37 Kidová et al. (2018) was used to generate the orthomosaic in six steps. In step 1, the
38
39 alignment of the images was performed using the photo-triangulation process and
40
41 generation of a sparse point cloud, which defined the coordinate system of the terrain.
42
43 In step 2, the sparse point cloud generated in the previous step was densified for a more
44
45 detailed representation of the mapped area and was also referenced the SIRGAS 2000
46
47 Zone 23S local coordinate system. In step 3, a model was built that accurately
48
49 represented the three-dimensional mapped terrain. Thus, it was possible to represent the
50
51 digital surface model (DSM), and, after filtering the point cloud of the soil, it was
52
53 possible to visualize the digital terrain model (DTM). In step 4, the texture was applied
54
55 to the model obtained in the previous step to improve the visual appearance and
56
57 distinction between objects. Step 5 consisted of the creation of the DEM. The generated
58
59
60

1
2
3 products were two-dimensional raster format representations of the DSM and DTM.
4
5 Lastly, the orthomosaic was generated in step 6.
6
7

8 9 ***Precision Assessment***

10
11
12 The process of geometric correction in images using GCPs consisted of a two-
13 dimensional transformation, in which the coordinates collected in the pixel were
14 replaced with the coordinates of the points obtained by receivers (GNSS) in the field
15 (Tawfeik, Elhifnawy, & Shawky, 2016).
16
17
18
19
20
21

22
23 The orthomosaics for the altitudes of 30, 60, 90, and 120 m were georeferenced
24 by PhotoScan 1.4.3. In this phase, the processed points obtained by the GNSS were
25 exported in a txt file and later loaded into the PhotoScan program, thereby allocating
26 GCPs at each georeferenced target position, so there was a combination of images with
27 the same coordinate system. In this process, unfocused images or poorly positioned
28 images in the photogrammetric alignment were relocated with greater precision, and
29 differences are presented as root mean square error (RMSE).
30
31
32
33
34
35
36
37
38

39
40 RMSE is commonly used to express numerical accuracy results. It has the
41 advantage of presenting values of errors in some dimensions of the analyzed variable
42 (Hallak & Filho 2011). It was considered an accuracy check to generate the RMSE data.
43
44 This approach consists of validating the adjusted coordinates using independent
45 georeferenced points. Each independent coordinate served as support to the studied
46 GCP. The values used to calculate the total root mean square error (RMSEt) were the
47 summation of the RMSE coordinate axis (X, Y, and Z), obtained by PhotoScan, and the
48 calculation was performed using Equation 1.
49
50
51
52
53
54
55
56
57
58
59
60

$$RMSE_t = \sqrt{\frac{\sum_{i=1}^n [(X_{O_i} - X_{GNSSi})^2 + (Y_{O_i} - Y_{GNSSi})^2 + (Z_{O_i} - Z_{GNSSi})^2]}{n}} \quad (1)$$

where n is the number of GCPs; X_{O_i} , Y_{O_i} , and Z_{O_i} are the X, Y, and Z coordinates that were respectively measured in the DEM; and X_{GNSSi} , Y_{GNSSi} , and Z_{GNSSi} are the X, Y, and Z coordinates that were respectively measured with the GNSS in the field.

The RMSE_t value was used to compare all 144 photogrammetric projects obtained from 399 aerial photos in this study.

Statistical Analysis

A response surface was obtained to represent the experimental data statistically using OriginPro 17 software. Response surface methodology (RSM) is one of the most widely used multivariate techniques to optimize processes (Ronix, Pezoti, Souza et al., 2017; Nasri & Mozafari, 2018). Based on the adaptation of a polynomial model to the experimental data, it is possible to predict the responses for all possible combinations of factors within a chosen experimental group (Bezerra, Santelli, Oliveira et al., 2008), thereby determining a regression model to optimize an output variable, which is influenced by independent variables (Behera, Meena, Chakraborty et al., 2018).

The values of the response variable (error) were plotted according to the sources of variation (altitude and density of points) on a three-dimensional graph of X (number of points in each distribution), Y (flight altitude), and Z (RMSE_t). Then, a response surface was calculated to better represent each “position”, as well as the surface equation and its respective correlation values.

Results and Discussion

The results of the initial post-flight parameters based on the different flight altitudes are provided in Table 2. For altitudes of 30 to 120 meters, the flight time ranged from 2 to 12 min. However, between the altitudes of 60, 90, and 120 m, the variation was only 2 min.

[Table 2 near here]

The existence of a linear correlation between flight altitude, number of images, and spatial resolution is shown in Table 2, confirming that the higher the number of images collected, the better the spatial resolution results. This phenomenon, which was observed by Mesas-Carrascosa, García, De Larriva et al. (2016) revealed that spatial resolution was directly related to flight altitude and could be predefined to achieve greater detail in orthomosaic images.

As presented in Table 2, the 60 m flight exhibited the highest efficiency among the altitudes assessed, collecting 86 images in four minutes. When compared to the other flights, this altitude exhibited significantly interesting values regarding flight time, number of images, and spatial resolution. This superior performance may be related to the focal length of the sensor, the size of the analyzed area, and the flying height, thereby promoting the best use of complete images.

Perroy, Sullivan, & Stephenson (2017) revealed the importance of flight altitude on the identification of species of trees in a forest compared to field sampling, concluding that as a flight reached higher altitudes, the possibility of correct identification decreased. In 2016, Quirós and Khot developed research relating flight altitude to the precision of counting plants in nurseries, highlighting the importance of flight altitude in the quality of the images and pointing out that above 40 m altitude, considerable errors were present in the plant counting results.

1
2
3 When observing the error presented by the different distributions studied
4 (distribution of GCPs and flight altitude) (Figure 6), the low interference of flight
5 altitude concerning georeferencing errors is evident. This analysis made it possible to
6 identify the distribution that least met the proposed objectives. Figure 6 shows that the
7 central distribution differed from the others, displaying errors of up to 0.12 m with the
8 30 m flight, which was above the mean of residual errors found in the other
9 distributions.

10
11
12 [Figure 6 near here]

13
14 It is also possible to see in Figure 6 the low performance of the center
15 distribution. It is worth mentioning that the increase in flight altitude favored the
16 decrease of RMSEt for this distribution. This situation occurred due to the reduction in
17 the number of images, consequently increasing the number of georeferenced points in
18 the orthomosaic. Furthermore, it was observed that the increase in flight altitude
19 promotes a reduction in RMSEt. Son et al. (2019) studied the flight parameters and
20 GCPs in the geometric quality of the orthomosaic obtained by a UAV and found better
21 values of RMSEt in flight altitudes between 80 and 150 m.

22
23 Opposite results of RMSEt values were found at different altitudes without the
24 use of GCPs. Rossi et al. (2017) observed that RMSEt errors were caused by factors
25 such as flight altitude, lack of oblique images, low-cost camera, or higher relief. Given
26 this, there are some contradictions for different sensors and types of terrain; however, in
27 this study, good relationships were found between flight altitude and GCP distribution
28 (Figure 6).

29
30 Based on the results presented in Figure 7, the density of GCPs per hectare could
31 be defined. Between 14 and 20 GCPs, a low variation in RMSEt values was verified. It
32 was possible to observe that above 14 CGPs, the RMSEt values reduced by only 2mm.

1
2
3 The stability between 14 and 20 points in this study area was verified, and millimeter
4 differences were observed in this interval. According to these observations, it was
5 determined that no more than 14 GCPs were needed for any distribution studied in this
6 work; therefore, it was possible to define a maximum of seven GCPs per hectare in
7 fieldwork for flights above 30 meters. In 2017, Agüera-Vega, Carvajal-Ramírez, and
8 Martínez-Carricondo showed that horizontal and vertical precision improved as the
9 density of GCPs increased and also found a limit of GCPs where the RMSEt values
10 were shown to stabilize.
11
12
13
14
15
16
17
18
19
20

21 [Figure 7 near here]
22

23
24 Based on the results presented in Table 3, the desired precision may be inferred
25 for any distribution between altitudes of 30 to 120 m, with GCPs varying between 4 to
26 20 points. RMSEt values can be estimated before executing a flight mission through
27 multiple nonlinear regression (Equation 2), where Z is the desired RMSEt. Thus, the
28 values of the parameters shown in Table 3 added in Equation 2 are represented in Figure
29 8 where X is the quantity of GCPs and Y represents the flight height.
30
31
32
33
34
35
36
37

$$38 \quad Z = Const + x + y + xy + x^2 + y^2 + x^2y + y^2x + x^3 + y^3 \quad (2)$$

39
40
41

42 The correlation coefficient values (R^2) range between 0.72 and 0.86, thereby
43 demonstrating the reliability of the presented calculations.
44
45

46 [Table 3 near here]
47

48 Figure 8 shows the interactions between the independent variables, flight
49 altitude, and density of GCPs, where the low RMSEt values are represented by cold
50 colors (blue) and the highest error values are represented by warm colors (red). The X-
51 axis shows the density of points for any distribution stabilized with 14 GCPs at
52
53
54
55
56
57
58
59
60

1
2
3 approximately 7 GCPs per hectare, thereby validating the information presented in
4
5 Figure 7.
6

7
8 Figure 8 shows that the results related to flight altitude for the diagonal and edge
9
10 distributions behaved similarly. As shown in Figure 5, the diagonal distribution covered
11
12 much of the border regions, thus providing similar characteristics to the graph presented
13
14 in Figure 8.
15

16
17 [Figure 8 near here]
18

19
20 As shown in the surface response graphs in Figure 8, the distribution of points in
21
22 the central region of the area resulted in the highest RMSEt values, with the error
23
24 reaching 20 cm in the 30 m flight altitude.
25

26
27 When compared to the 60, 90, and 120 m flight altitudes, this error tended to
28
29 decrease because, at higher altitudes, the sensor collected fewer images (Table 2), which
30
31 increased the density of points per image and improved adjustments via GCPs.
32

33
34 As seen in Figure 8, the best RMSEt results were expressed in the parallel
35
36 distribution, possibly because this distribution model georeferenced images from the
37
38 center to the edge distribution in a constant manner, thus covering a greater number of
39
40 targets per captured image. The response results of the parallel distribution behaved in a
41
42 way that improved the RMSEt by increasing the flight altitude. Figure 8 shows that the
43
44 RMSEt values ranged from 3 to 7 cm, respectively, between 30 and 120 meters.
45

46
47 This research showed that flight altitude influenced RMSEt values, thereby
48
49 counter-corroborating the results of Gómez-Candón, De Castro, & López-Granados
50
51 (2013), who concluded in their research that flight altitude was an important parameter
52
53 to consider when acquiring images using an UAV. However, they found no differences
54
55 in the RMSEt georeferencing in the orthomosaics created by UAVs between 30 and 100
56
57 m high.
58
59
60

1
2
3 Figure 8 shows that some distributions presented similarity between the graphs.
4
5 Distributions such as diagonal, parallel, and stratified presented smaller RMSEt values,
6
7 potentially because of the distribution pattern, i.e., the spacing between each GCP
8
9 followed a uniform alignment for each direction, allowing the GCPs to be well-
10
11 distributed in the area. The influence of a poor distribution of GCPs was described in
12
13 the research of Sanz-Ablanedo, Chandler, Rodríguez-Pérez et al. (2018), who
14
15 demonstrated that GCPs should be evenly distributed throughout the area of interest,
16
17 ideally in an angular grid, because any GCP is minimized with maximum distance.
18
19 These results indicated that, for a given density of GCPs, the precision obtained using
20
21 optimal distribution would be twice as good as when GCPs were poorly distributed.
22
23
24
25

26 In the work of Martínez-Carricondo, Agüera-Vega, Carvajal-Ramírez et al.
27
28 (2018), the authors suggested that to achieve more accurate values in orthomosaic
29
30 georeferencing, GCPs should be distributed along the study area border in a stratified
31
32 manner. However, Figure 8 shows a better distribution of the GCPs whereby parallel
33
34 distribution was the most suitable for generating smaller error, i.e., below 7 cm and with
35
36 a correlation coefficient of $R^2 = 0.83$, potentially due to a more uniform distribution
37
38 among the models considered.
39
40
41

42 The center, edge. and random models exhibited higher RMSEt results, possibly
43
44 due to the poor distribution of the GCPs and fewer points per image. Figure 8
45
46 demonstrates the low performance of the center distribution; at any flight altitude, this
47
48 type of distribution georeferenced fewer images, as the number of points were clustered
49
50 in the middle of the area.
51
52

53 Figure 9 shows that as a flight increased in altitude, all distributions increased
54
55 the number of GCPs per images because the number of images decreased as flight
56
57 altitude increased (Table 2). Therefore, the greater points density per image, the better
58
59
60

1
2
3 the geometric precision. For example, in the central distribution, which was considered
4 the least precise distribution, as the altitude increased the number of GCPs increased as
5 well, and the error decreased. This is because, in high flight altitudes for this
6 distribution, it is possible to observe GCPs in the image center and also on the edge of
7 the image. This was shown by the 120 m altitude flights.
8
9

10
11
12
13
14 [Figure 9 near here]

15
16 As noted in Figure 9, the number of points per image tended to stabilize above
17 12 GCPs or six GCPs per hectare, or when the flight altitude exceeded 100 m, thereby
18 corroborating the above discussion regarding the number of points per image. In the
19 center distribution, as the number of points increased, the errors decreased, which
20 caused the additional points to reach other images. Considering a spacing of 20 m at an
21 altitude of 120 m, the center points may have georeferenced the edge images, which did
22 not occur at low altitudes such as 30 m.
23
24
25
26
27
28
29
30
31
32

33 Mission planning prior to flight execution and field checkpoint surveys
34 contribute to the objectivity of the work by reducing costs and operating time. In this
35 research, the distribution of GCPs in the field and the previous adjustment of flight
36 altitude were shown to contribute to a reduction in the number of GCPs and to
37 achieving the previously defined RMSEt. Knowledge of the sensors attached to the
38 aircraft enables more efficient missions regarding flight time.
39
40
41
42
43
44
45
46
47

48 **Conclusion**

49
50 The most efficient altitude was 60 meters when considering the number of images and
51 flight time. Based on the surface response analysis, the central distribution of GCPs was
52 observed to have low precision. To achieve geometric precision below 0.07 m for
53 stratified and random edge distributions, 10 GCPs at any flight height are
54 recommended. However, for studies requiring up to 0.07 m precision, the best
55
56
57
58
59
60

1
2
3 distribution was parallel with four GCPs at any altitude. The diagonal positioning of the
4
5 GCPs showed RMSEt values below 0.11 m with four GCPs at any altitude. Despite
6
7 good relationships between GCP density and distribution for the precision range, the
8
9 number of image points had a greater influence on the georeferencing of the
10
11 orthomosaic.
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60

For Peer Review Only

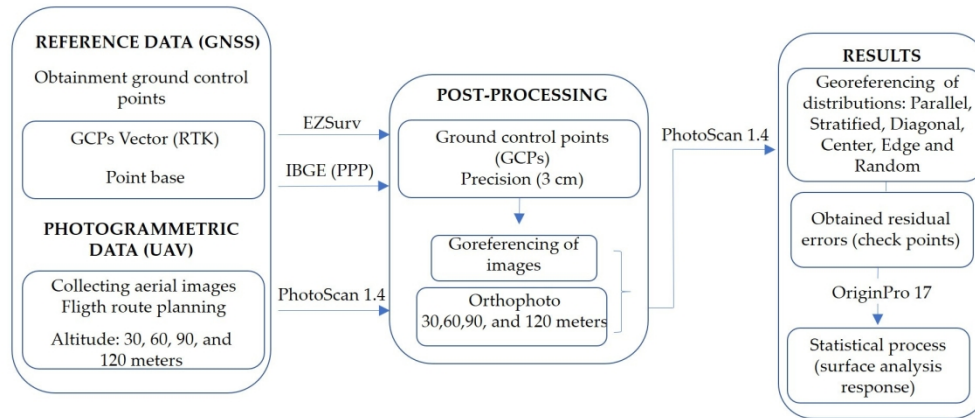


Figure 1. Flowchart of methodological processes.

161x71mm (300 x 300 DPI)

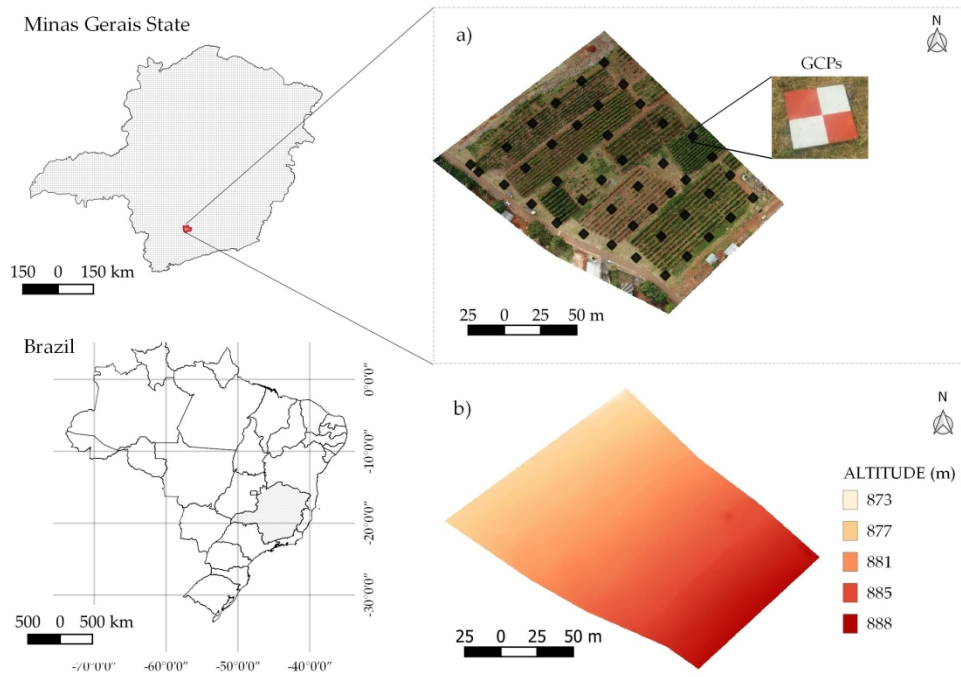


Figure 2. Location of the study area. A) The positions of ground control points (GCPs) tracked through global navigation satellite system GNSS and detail of the plate representing a GCP. b) Digital terrain model (DTM).

209x147mm (300 x 300 DPI)

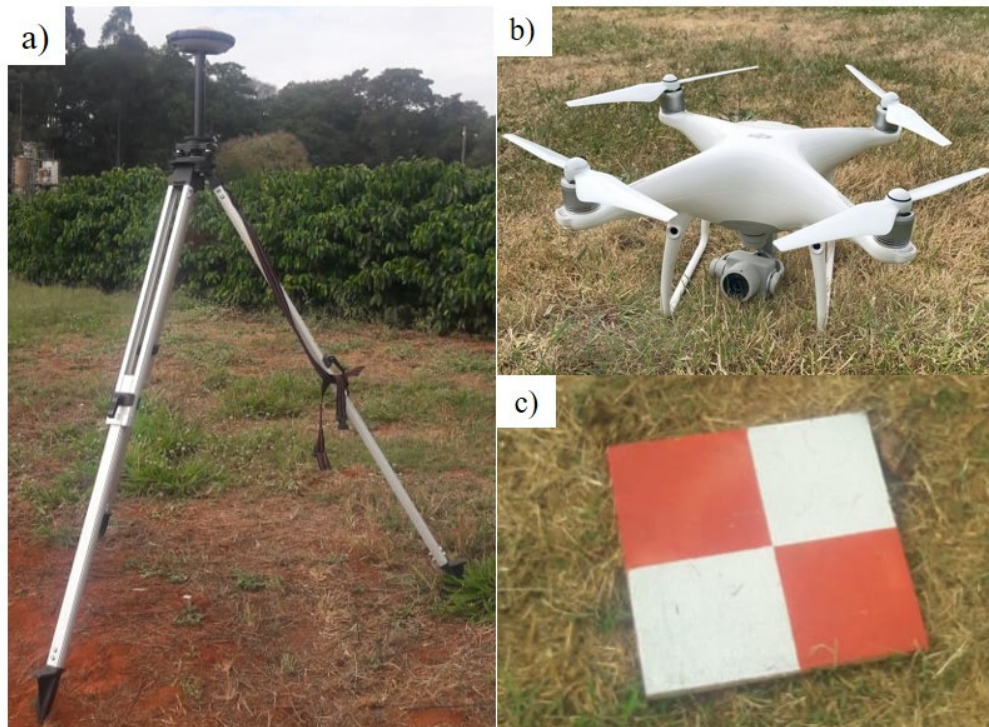


Figure 3. a) GNSS receiver; b) unmanned aerial vehicle (UAV); c) 0.30 x 0.30 m GCP.

67x49mm (300 x 300 DPI)

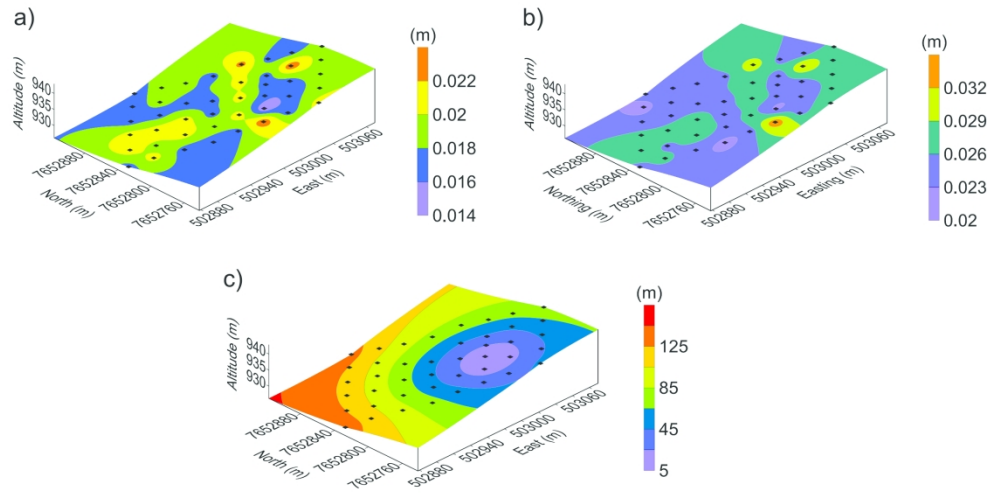


Figure 4. GNSS (Rover) geometric coefficients measurements obtained by coordinate adjustment. a) Vertical precision (m); b) horizontal precision (m); c) ellipsoidal distance (m).

224x114mm (300 x 300 DPI)

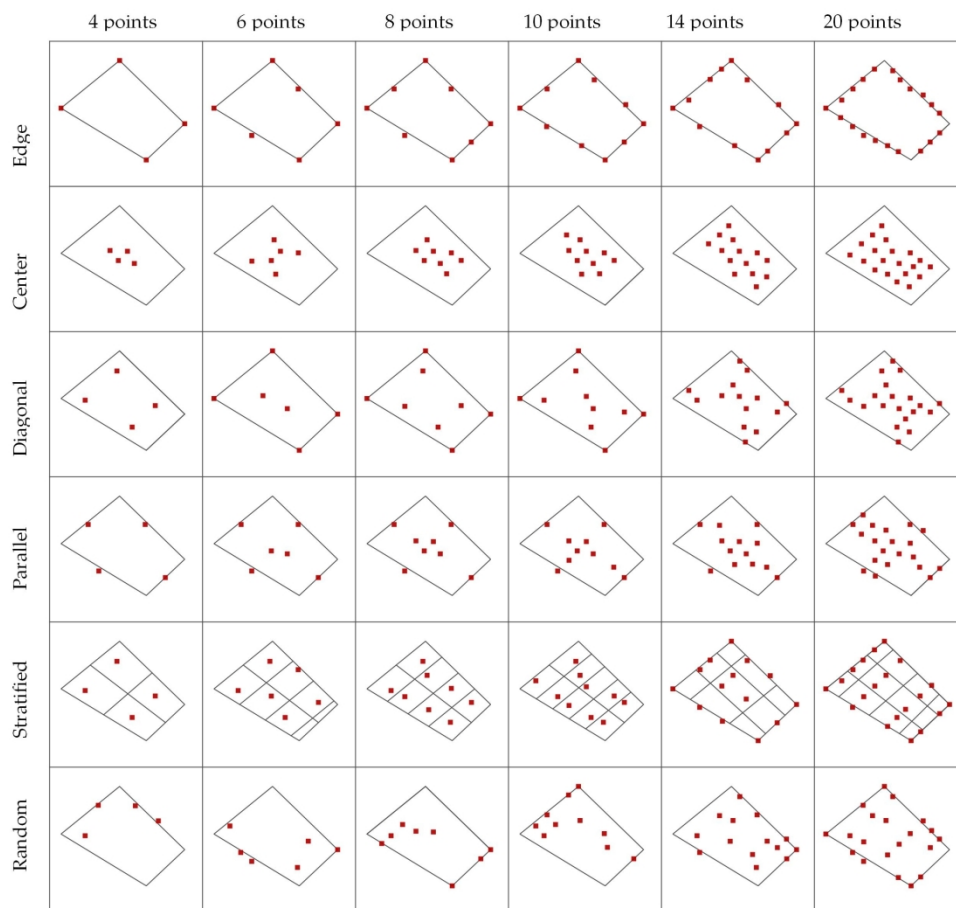


Figure 5. GCPs combination where the x-axis represents the GCPs density and the y-axis represents the GCPs distribution.

219x209mm (300 x 300 DPI)

1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60

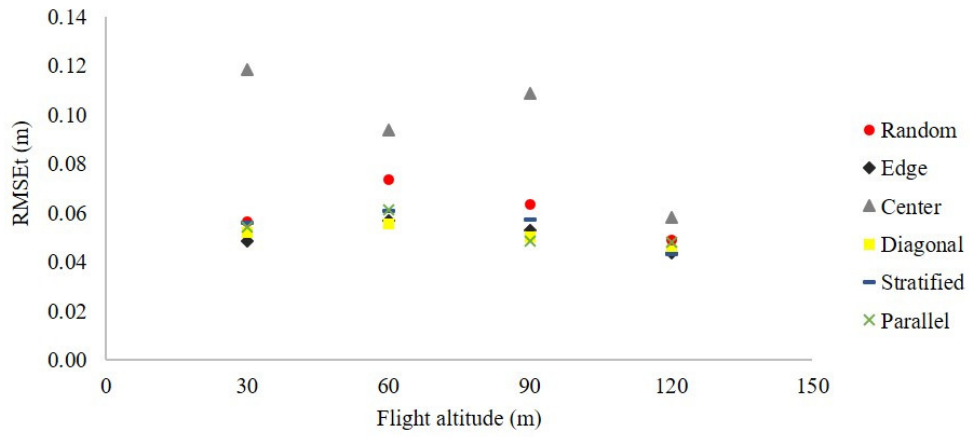


Figure 6. Total root mean square error (RMSEt) (m) value according to the different distributions of GCPs and different flight altitudes.

78x36mm (300 x 300 DPI)

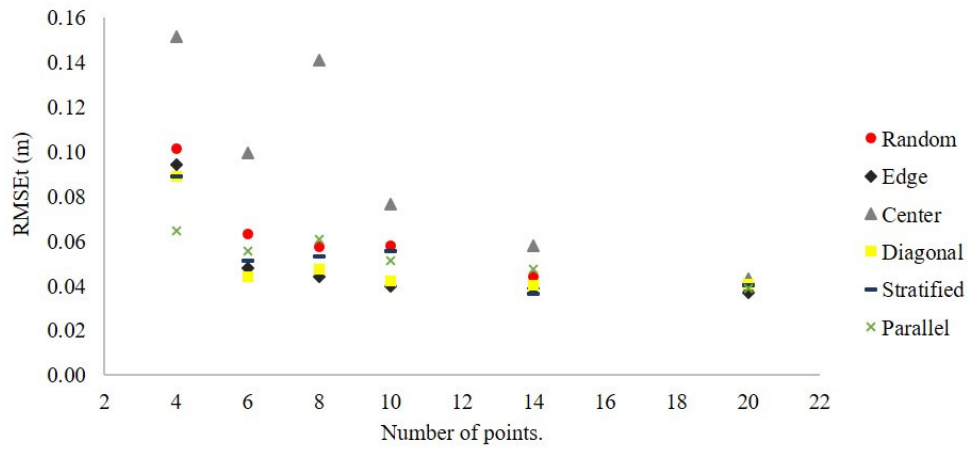


Figure 7. Variation in RMSEt distribution of flight altitudes for density of GCPs.

79x38mm (300 x 300 DPI)

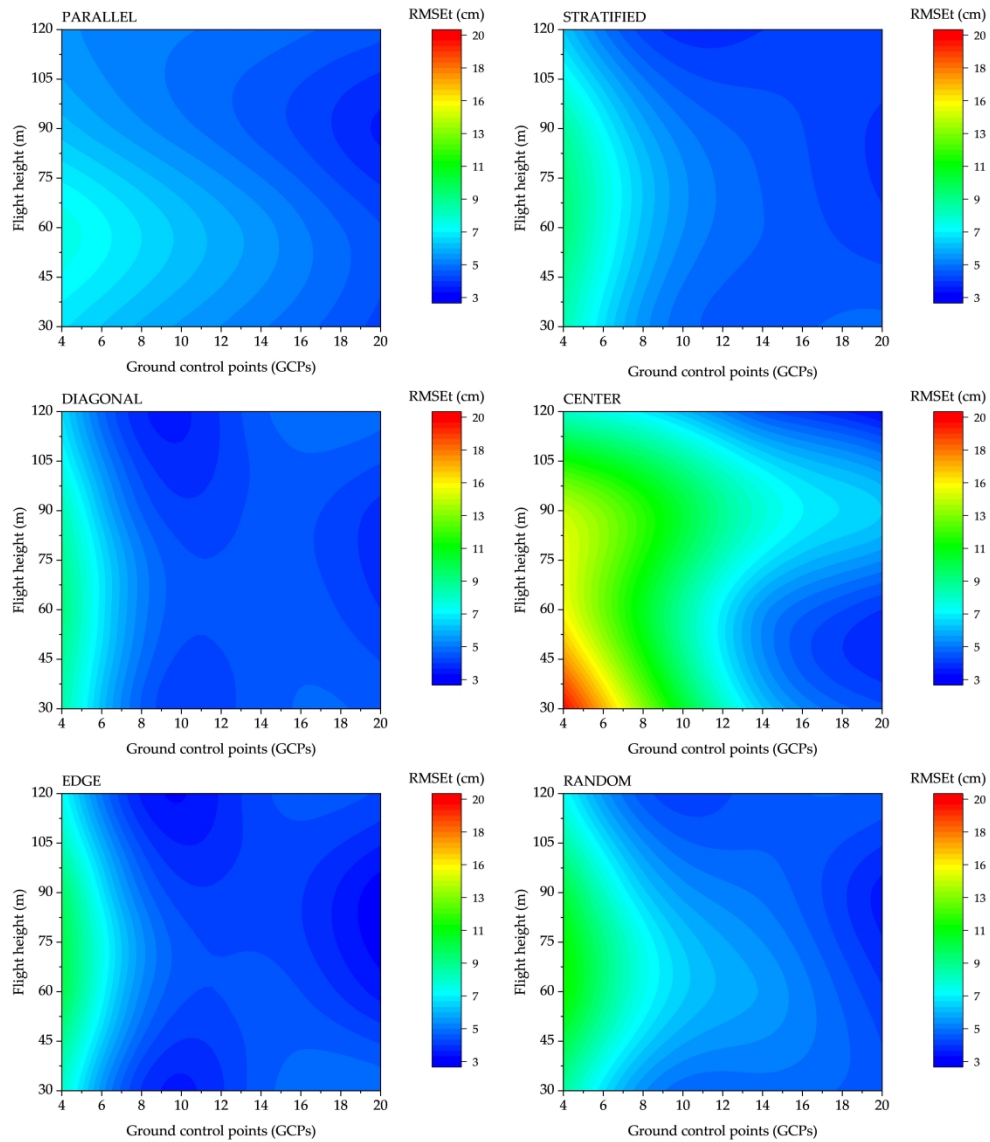


Figure 8. Response surface graphs for each distribution. The x-axis represents the density of GCPs, the y-axis represents the flight altitude, and the color variation refers to the total root mean square error (RMSEt).

149x171mm (768 x 768 DPI)

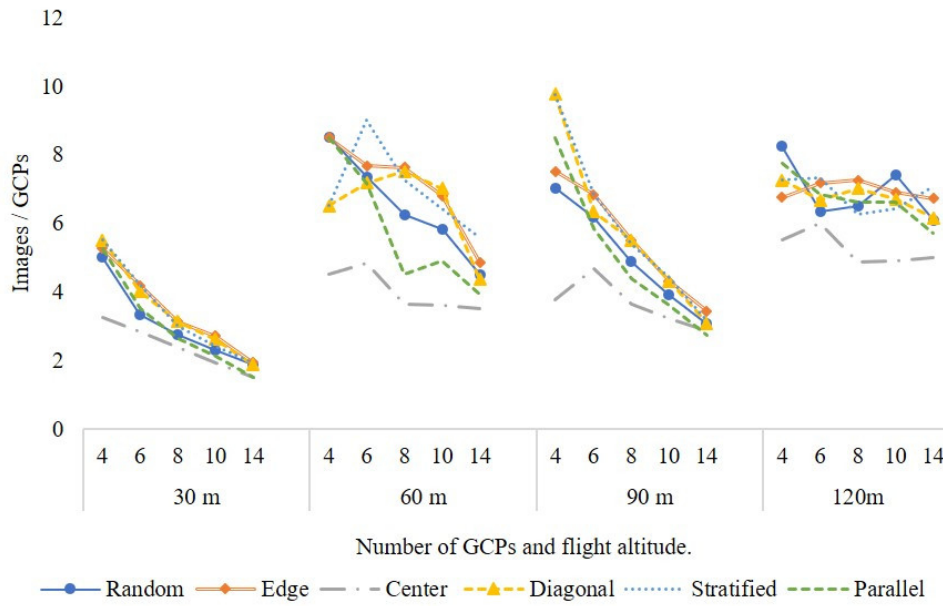


Figure 9. Number of images per GCP for each distribution considering flight altitudes of 30, 60, 90 and 120 m.

76x48mm (300 x 300 DPI)

Table 1. IBGE platform post-processing GNSS (BASE) data.

	Latitude (gms)	Longitude (gms)	Alt. Geo. (m)	UTM N (m)	UTM E (m)
Sirgas 2000	-21° 13' 35,2339"	-44° 58' 15,5406"	937,81	7652789,482	503011,078
Survey*	-21° 13' 35,2269"	-44° 58' 15,5423"	937,81	7652789,697	503011,03
Sigma (95%)	0,004	0,008	0,009		
Model Geoidal	MAPGEO2015				
Ondul. Geoidal (m)	-3,97				
Alt. Ortométrica (m)	941,78				
Central meridian	-45				

Table 2. Flight parameters and initial mission results.

Altitude	Number of images	Flight time (min)	cm/pixel
30	242	12	0.68
60	86	4	1.44
90	44	3	2.26
120	27	2	2.94

For Peer Review Only

Table 3. Calculated values to obtain the RMSEt based on the altitude values (Y) and the density of GCPs (X).

Parameters	Random	Edge	Center	Diagonal	Stratified	Parallel
constant	6.30E-02	1.31E-01	4.74E-01	1.62E-01	1.18E-01	6.54E-03
x	-2.61E-02	-3.99E-02	-2.06E-02	-3.82E-02	-2.12E-02	-2.61E-03
y	5.38E-03	3.43E-03	-1.08E-02	1.98E-03	1.62E-03	3.80E-03
x ²	2.29E-03	3.55E-03	-2.58E-04	3.08E-03	1.57E-03	1.62E-04
x*y	-1.96E-04	-1.90E-04	2.41E-04	-7.24E-05	-8.90E-05	-4.81E-05
y ²	-5.51E-05	-2.97E-05	1.39E-04	-2.22E-05	-1.25E-05	-5.25E-05
x ³	-5.43E-05	-8.54E-05	2.89E-05	-7.29E-05	-3.27E-05	-3.41E-06
x ² *y	-2.59E-07	-8.37E-07	-6.13E-06	-1.31E-06	-1.29E-06	-3.52E-07
x*y ²	1.43E-06	1.40E-06	-1.29E-07	8.02E-07	8.77E-07	4.58E-07
y ³	1.40E-07	4.60E-08	-6.45E-07	4.98E-08	-7.85E-09	2.03E-07
R ²	0.86	0.72	0.74	0.79	0.78	0.83