Multiscale and Multiphysic Simulation of Electric Vehicles in Real Time Applications

Lorenzo Berzi¹, Tommaso Favilli¹, Edoardo Locorotondo¹, Marco Pierini¹, Luca Pugi¹

¹University of Firenze, Italy, e-mail:Luca.Pugi@unifi.it

Abstract. Modern electric vehicles are complex mechatronics systems whose behaviour is highly influenced by the concurrent action of mechanical and electrical systems interfaced with complex control logics aiming to improve several aspect concerning energy management, vehicle stability, comfort and guidance. As a partner of the European Project Obelics (Optimization of scalaBle rEaltime modeLs and functIonal testing for e-drive ConceptS), authors have focused their attention in system integration and model optimization of powertrain systems with a particular attention to the problem of brake blending respect to different applications (smart energy management, vehicle stability, hardware in the loop testing of connected mechatronics systems). In this work authors introduce main features and possible usages of brake models that they have to develop within the Obelics Project. Proposed models have to be implemented and verified also for realtime implementation with a particular attention to RT-Implementation and Co-Simulation with models provided by the other partners of the project. For this reason, authors introduce specifications concerning Real Time implementation not only in terms of scheduling of different tasks but also proposing a reference architecture of Real Time controller (An hybrid multi-core systems with on board FPGA) that should be used for the preliminary prototyping and testing of the proposed models. Finally, a preliminary "toy", simplified model is proposed in order to verify the feasibility of the proposed architecture respect to a future complete implementation and integration with the product of the research of the other partners of the project.

Keywords: Mechatronics, Real-Time Simulation, Multi-Scale Models, Multi-Physics Models, Brake Blending

This document has been made available as post print version on Institutional repository – FLORE (University of Florence).

1 Introduction: Brake Blending, State of The Art and Involved Research Activities

Authors are members of a research team of Università degli Studi di Firenze, that are partner of the Obelics [1] (Optimization of scalaBle rEaltime modeLs and functIonal testing for e-drive ConceptS). In order to positively contribute to the project authors are focusing their attention on the problem of the brake blending in road electric vehicles. Brake blending is a classic topic in railway engineering [2-3] where electric and conventional braking are often applied simultaneously in order to obtain an optimization of maintenance costs (reduction of wear and loads to which are subjected friction components of conventional brakes) and an improvement of energetic efficiency allowing a regenerative transfer of the braking energy through the overhead lines to other available loads represented by other trains on the same line or (more recently) by static infrastructures, such as reversible power stations or energy storage systems[4]. If external loads for regenerative braking are not available, railway vehicles are also equipped with internal resistors to perform on board dissipative electric braking.

The term blending is used to indicate the control criteria of both conventional and electric braking that is implemented in order to assure desired braking performances avoiding any undesired dynamical effect that should arise from the contemporaneous application of braking forces produced different systems [5].

On road electric vehicles optimization of electric blending is further complicated by the fact that exerted braking efforts also influence vehicle lateral stability. Also modulation of braking forces is often used by on board control subsystems such as ESP(Electronic Stability Program)[6] or other torque vectoring systems to stabilize the trajectory of the vehicle.

Also application regenerated energy have to be stored on vehicle accumulators which should not be able to manage required power transfer[7-8], as example if the state of charge is too high or involved currents should be higher respect to known safety limits of the storage. In all these conditions even if the electric powertrain is completely efficient, regenerative braking efforts cannot be applied, so this potential unavailability has to be managed by the brake blending controller in order to produce a reliable behavior of the system. Finally, it should be noticed that the dynamical response of electric motors/actuation systems are much faster and more controllable respect to conventional internal combustion engines so electric traction motors should be used to perform a fast and precise multi-quadrant control of the exerted torques contributing to modulate longitudinal efforts on wheels contributing enhanced behavior of board on subsystem ABS(Antiblockiersystem)ASR(Acceleration Slip Regulation // Anti-Slip Regulation)[9], ESP and other torque vectoring controls that are usually performed on conventional vehicles wireless vehicles. In literature [10-12] there is a wide variety of studies considering possible implementations of advanced control

This document has been made available as post print version on Institutional repository – FLORE (University of Florence).

Final published version is available at: https://doi.org/10.1007/978-3-030-03320-0 15

1

techniques aiming to exploit the possible advantages deriving from superior dynamic performances of electric motors.

This is should be very interesting also considering the possible implementation of this mechatronic subsystems to vehicle with multiple traction motors or direct drive inwheel solution that should be promising almost both for off-road applications or urban mobility as visible in the scheme of figure 1 where different examples [1215] are introduced.



Fig. 1 Examples of multiple electric motors and electric powertrains, a) a conventional layout with multiple motors connected by MRTTM(Multiple Rotor Transmission)[12-13], b)

Advanced Torque Vectoring with multiple electric motors by Honda [14], c) an example of four in-wheel vehicle [15]

Finally, it's interesting to notice another interesting topic related to brake blending which is directly connected with the more recent developments of high frequency inverters and energy storage management systems: high levels of reliability of energy storage systems involves a constant monitoring of high frequency interactions with traction motors and drive systems [16]. In particular, it should be interesting to verify the behavior of the system when complex control tasks are performed by traction motor (as example high frequency modulation of exerted torques for torque vectoring) also it should be interesting to verify if the frequency content associated to this behavior should be exploited to perform diagnostic identification procedures aiming to verify the current state of health of energy storage systems implementing on line spectroscopic identification procedures[17].

2 Proposed Task Partitioning and Hardware Implementation for a Modular Real-Time Simulation

As briefly explained in the introduction, advanced simulation of brake blending is a typical example of multi-scale multi-physics phenomena involving the interaction between different simulation subsystem whose main features are briefly described in Table 1. In particular, for the design of a modular simulation platform some preliminary evaluations from Table 1 should be quite useful:integration frequencies that should be needed to reproduce the High frequency response of power electronic systems should be really high for real time implementation and difficult to be implemented directly on a RTOS (Real Time Operating System) not only in terms of computational load but also in terms of jitter of the system. Also management of I/O signals from external measurement or actuation devices (as example for Hardware in the Loop or Software in the Loop applications) should be relatively simpler with FPGA(Field Programmable Gate Array).

This document has been made available as post print version on Institutional repository – FLORE (University of Florence).

Final published version is available at: https://doi.org/10.1007/978-3-030-03320-0_15

Electric Motor and Drives

Battery Models

Low Lev. Control of Power Devices

Efficiency, Thermal and Wear Models Thermal/

Considering variety and number of implemented subsystems that should be implemented a modular structure and a discrete partitioning [18] between different tasks running on different threads should be quite mandatory. Many modern real tools available in commercial products (as example from MatworksTM or from National Instruments[™]) allow some automatic or smart distribution of concurrent tasks between different cores. However, a good organization of tasks should be fundamental to optimize the execution of the system. In this work authors adopted a physical based distinction between "Continuous" and "Discrete" subsystems. Continuous models represent physical systems whose mutual interaction has to be modelled minimizing delays introduced by the execution on a real time target which is necessary discrete.

Physical Continuous/Discrete System Mean Integration Description Domain (Num.Stiffness) freq. (ODE1 solver) Multibody Vehicle Model Mechanical Continuous*(Stiff) 103-104[Hz] Tire/Road Contact Models Mechanical Continuous*(Stiff) 103-104[Hz] 10³-10⁴[Hz] Hydraulic Plant/Brake Models Mainly Fluid Continuous*(Stiff) On board Digital Control Systems Math/Digital Discrete (Not stiff) Typ. 10¹-10³[Hz]

Continuous (Stiff)

Discrete (not Stiff)

Continuous*(Stiff)

Continuous*(Not Stiff)

10⁵-10⁹ [Hz]

10³-10⁶[Hz]≠ 101-102[Hz]

104[Hz]

Table 1. Simulated Dynamical Behavior and corresponding integration features

For batteries integration sampling frequency is strongly influenced by the kind of adopted model and its potential usage to investigate (or not) high frequency interactions with coupled electrical systems

Electric

Other

Math/Digital

Electro-Chem.

Computational delays (due to task execution and data exchange between different tasks) are tolerable only if they are relatively negligible respect to the typical time scale of the phenomena that they have to reproduce. For this reason, in Table 1 some consideration concerning the mean integration time needed to correctly reproduce a desired dynamic are shown. Obviously it should be easier the decoupling and the implementation on different tasks of slow processes such as thermal and wear models since delays introduced by data exchange with faster models should produce relatively small consequences on simulation accuracy.

On the other hand, the model has to reproduce control algorithm and other processes that are discrete also in the real world. In this case the correct implementation of delays associated to data acquisition, communication and production of outputs are mandatory to correctly reproduce the dynamical behavior of the system but at the same time their correct implementation is also useful to perform a discrete task partitioning since delays that have to be reproduced to fit a real physical behavior

This document has been made available as post print version on Institutional repository – FLORE (University of Florence).

Final published version is available at: https://doi.org/10.1007/978-3-030-03320-0 15

⁽friction and power components) *All physical Systems are "Continuous" while discrete systems are typically represented by digital control systems to which is typically associated an execution sampling rate. When performing simulation with fixed step integrators, execution frequency of digital systems should be at least a magnitude order slower respect to the corresponding integration frequency of coupled continuous systems in order to avoid the risk of unrealistic coupling effects between systems that are modelled with the same discrete sampling

should be used to manage communication and data exchange between different tasks on the real time platform. According to the above described specifications authors have selected a possible hardware for the preliminary real-time implementation of brake-blending models whose main data are described in table 2: it's interesting to notice that the proposed platform is substantially a hybrid multicore real-time controller with a Xilinx FPGA. In this way simulation of most demanding tasks (such as the electrical ones of Table 1) should be implemented on FPGA. Since the Real Time Controller has two cores, slower tasks and control ones allowing higher delays (such as simulation of digital systems in which I/O delays have to be reproduced) should be distributed in a core while some the others fastest ones should be executed by the other one.

Table 2. Specification of the RT Platform chosen for the preliminary real-time implementation and simulation of Brake Blending Models

Supplier/	Main Controller//	Slave-	Available I/O
Chosen Board	Slave-Comunication	FPGA	(For Exp. Activities)
dSpace/ MicrolabBox* *RT Target for Matlab-Simulink TM , Siemens Amesim TM	Freescale QorlQ P5020, dualcore, 2 GHz // QorlQ P1011 800 MHz , 2 Int. Ethernet interfaces (host+I/O), USB 2.0 ("flight recorder") and booting	Xilinx® Kintex®-7 XC7K325 T FPGA	ADC: 8 14-bit // 24 16-bit channels DAC: 16 16-bit channels DIO: 6 x Encoder//2 x Hall sensor input//2 x EnDat interface//2 x SSI interface//Sync. multi-channel PWM Block com.PWM// 2 CAN//2 x UART (RS232/422/485)// 1 x LVDS

All these design criteria are substantially summarized in the simplified scheme of figure 2: preliminary proposed configuration is relatively robust respect to delays introduced by data exchange between threads since it's optimized respect to the coupled dynamics of simulated systems.



Fig. 2 Chosen Hybrid Controller (Freescale-multi core-Power PC controller and FPGA) with corresponding task partitioning

2 Preliminary Implementation of a Simplified "Toy" Model: Some Results and Observations

According over-introduced specifications, authors have assembled a simplified "toy" model of a vehicle with its main sub-systems. Aim of this activity is to verify

This document has been made available as post print version on Institutional repository – FLORE (University of Florence).

Final published version is available at: https://doi.org/10.1007/978-3-030-03320-0 15

feasibility and functionality of the proposed approach while more complex models (developed by other partners of the project) are still not available, since the project is still in a preliminary phase. In particular authors, according project deliverables[19], are responsible for brake models visible in Figure 3. However, in order to properly simulate brake plant models also other interacting dynamical systems has to be simulated. In particular, simplified mechanical models of the vehicle (quarter vehicle and/or planar 7DOF one), tyre-road ones (Pacejka [20] models available in commercial softwares such a Matlab SimulinkTM or Siemens AmesimTM) and some simplified transfer functions able to simulate the behaviour of the electric powertrain. Also a simplified model of the energy storage system is introduced[21].

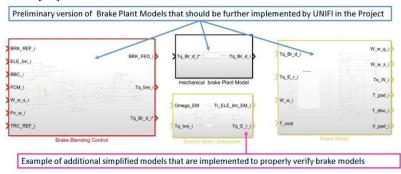


Fig. 3 Implemented brake models in Matlab-SimulinkTM (Atomic Subsystems discretized and implemented for RT implementation)

All the implemented models are integrated separately simulating different sampling frequencies and communication delays. In order to properly verify the portability of the code within different partners of the project each subsystems are compiled and transformed in discrete Matlab-Simulink S-functionsTM. This is also verification of code portability[22] that is preliminary to the conversion of proposed model in the FMI(Functional Mock-up Interface) the open universal co-simulation standard [23] to which have to converge all the models proposed in Obelics in order to assure a complete interoperability of the research products among all partners. In figure 4/a/b some preliminary results referred to the simulation of a braking maneuver of a simplified quarter vehicle model. In figure 4/c same simulation is repeated considering degraded road adhesion conditions. These results are quite interesting to verify model stability and reliability respect to delays and errors introduced by fixed step integrators (discrete or ODE 1 integration) and relatively large integrations steps (fastest tasks run at 10KHz but most of the model is successfully working with 100-1000Hz sampling frequencies). In particular, it's clearly noticeable the absence of "chatter" phenomena that are typically caused by delays introduced by discrete task partitioning in real time systems.

This document has been made available as post print version on Institutional repository – FLORE (University of Florence).

Final published version is available at: https://doi.org/10.1007/978-3-030-03320-0_15

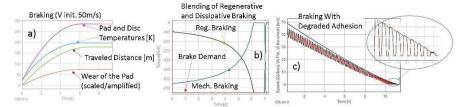


Fig. 4 example of preliminary simulation results, a) some results of braking simulations, b) blending between mechanical and Electrical Blending, c) braking with degraded adhesion conditions

6 Conclusions and Future Developments

In this work authors have introduced preliminary design activities concerning real time simulation and optimization of brake blending models produced by University of Florence. Most innovative and significant results of these activities mainly concerns implementation procedures aiming to assure portability of produced code within different partners and simulation environments. As further development author wish to be able to further customize and develop the model respect to Use Cases proposed by Industrial Partners of the Project (Example of advanced prototypes of Electric Vehicles that should be simulated using the proposed tools). Also in order to assure the prescribed portability of proposed models authors will verify also FMI implementation and compatibility with advanced models proposed by the other partner of the project.

Acknowledgments This work is part of the OBELICS project which has received funding from the European Unions Horizon 2020 research and innovation programme under grant agreement No. 769506.

References

- 1. Official site of the Obelics EU Project (https://obelics.eu/)
- Pugi, L., Malvezzi, M., Papini, S., Tesi, S. Simulation of braking performance: The AnsaldoBreda EMU V250 application (2015) Proceedings of the Institution of Mechanical Engineers, Part F: Journal of Rail and Rapid Transit, 229 (2), pp. 160-172. DOI: 10.1177/0954409713504394
- Pugi, L., Malvezzi, M., Conti, R. Optimization of traction and braking subsystems with respect to mission profile (2014) Civil-Comp Proceedings, 104
- Conti, R., Galardi, E., Meli, E., Nocciolini, D., Pugi, L., Rindi, A. Energy and wear optimisation of train longitudinal dynamics and of traction and braking systems (2015) Vehicle System Dynamics, 53 (5), DOI: 10.1080/00423114.2014.990466
- Leigh, M. J. (1994). Brake blending. Proceedings of the Institution of Mechanical Engineers, Part F: Journal of Rail and Rapid Transit, 208(1), 43-49.

This document has been made available as post print version on Institutional repository – FLORE (University of Florence).

Final published version is available at: https://doi.org/10.1007/978-3-030-03320-0_15

- Van Zanten, A. T. (2000). Bosch ESP systems: 5 years of experience (No. 2000-01-1633). SAE Technical Paper.
- Ren, G., Ma, G., & Cong, N. (2015). Review of electrical energy storage system for vehicular applications. Renewable and Sustainable Energy Reviews, 41, 225-236.
- 8. Lv, C., Zhang, J., Li, Y., & Yuan, Y. (2015). Mechanism analysis and evaluation methodology of regenerative braking contribution to energy efficiency improvement of electrified vehicles. Energy Conversion and Management, 92, 469-482.
- Huber, W., Jonner, W. D., & Demel, H. (1988). Simulation, performance and quality evaluation of ABS and ASR (No. 880323). SAE Technical Paper.
- Sawase, K., Ushiroda, Y., & Miura, T. (2006). Left-right torque vectoring technology as the core of super all wheel control (S-AWC). Mitsubishi Motors Technical Review, 18, 16-23.
- De Novellis, L., Sorniotti, A., Gruber, P., & Pennycott, A. (2014). Comparison of feedback control techniques for torque-vectoring control of fully electric vehicles. IEEE Transactions on Vehicular Technology, 63(8), 3612-3623.
- 12. Description of MRT™ freely available the the official site of the IET company http://www.ietspa.com
- Ceraolo, M., Lutzemberger, G., Sani, L., Valenti, G., Pretto, A., Pugi, L. Full electric and hybrid series vans: Cost, performance and efficiency evaluation for different powertrain layout (2017) 2017 International Conference of Electrical and Electronic Technologies for Automotive, art. no. 7993205, DOI: 10.23919/EETA.2017.7993205
- 14. Technical Documentation on hybrid solutions with torque vectoring performed with multiple electric motor available at the site of Honda Companyhttp://world.honda.com/Hybrid/
- Pugi, L., Grasso, F., Pratesi, M., Cipriani, M., Bartolomei, A. Design and preliminary performance evaluation of a four wheeled vehicle with degraded adhesion conditions (2017) International Journal of Electric and Hybrid Vehicles, 9 (1), pp. 1-32. DOI: 10.1504/IJEHV.2017.08281
- Doersam, T., Schoerle, S., Hoene, E., Lang, K. D., Spieker, C., & Waldmann, T. (2015, August). High frequency impedance of Li-ion batteries. In Electromagnetic Compatibility (EMC), 2015 IEEE International Symposium on (pp. 714-719). IEEE.
- Al Nazer, R., Cattin, V., Granjon, P., Montaru, M., & Ranieri, M. (2013). Broadband identification of battery electrical impedance for HEVs. IEEE transactions on vehicular technology, 62(7), 2896-2905.
- Gazzarri, J., Shrivastava, N., Jackey, R., and Borghesani, C., "Battery Pack Modeling, Simulation, and Deployment on a Multicore Real Time Target," SAE Int. J. Aerosp. 7(2):207213, 2014, https://doi.org/10.4271/2014-01-2217.
- OBELICS Project deliverable D3.1: Standardized model integration, https://obelics.eu/download/project_results/OBELICS-D3.1-Standardized-ModelIntegration.pdf
- 20. Pacejka, H. (2005). Tire and vehicle dynamics. Elsevier.
- E. Locorotondo, L.Pugi, L.Berzi, M. Pierini, G. Lutzemberger, Online identification of Thevenin equivalent circuit model parameters and estimation State Of Charge of LithiumIon batteries, Proc. of the 18th IEEE EEIC Int. Conference on Environment and Electrical Engineering, Palermo 12-15 June 2018.
- Stettinger, G., Benedikt, M., Thek, N., & Zehetner, J. (2013). On the difficulities of realtime co-simulation. V International Conference on Computational Methods for Coupled Problems in Science and Engineering, COUPLED PROBLEMS 2013. Ibiza, Spain.
- The Functional Mock-up Interface Standard. (n.d.). Retrieved from http://fmistandard.org/downloads/

This document has been made available as post print version on Institutional repository – FLORE (University of Florence).

Final published version is available at: https://doi.org/10.1007/978-3-030-03320-0 15